

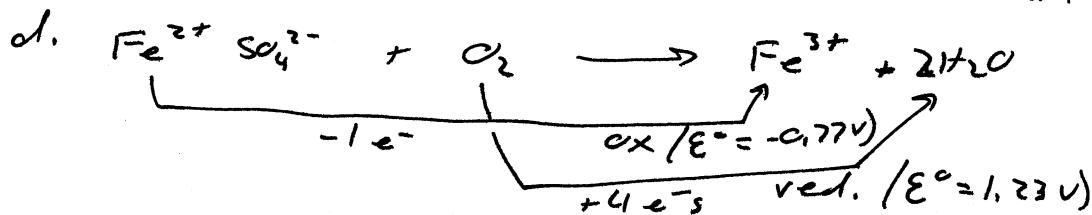
1. Ch 11, 34.c. Ag + CuCl₂ rxn?

Ag metal can be oxidized to Ag⁺ ($E^\circ = -0.80\text{ V}$)

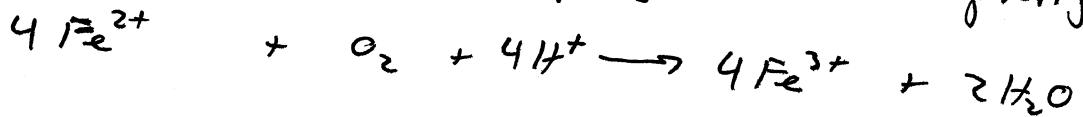
Cu²⁺ can be reduced to Cu⁺ ($E^\circ = +0.16\text{ V}$)

or to Cu metal ($E^\circ = +0.34\text{ V}$)

neither option provides a positive E_{cell}° , so no rxn.



Let's balance this first... (dropping the SO₄²⁻ for simplicity)

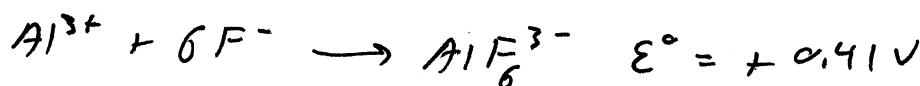
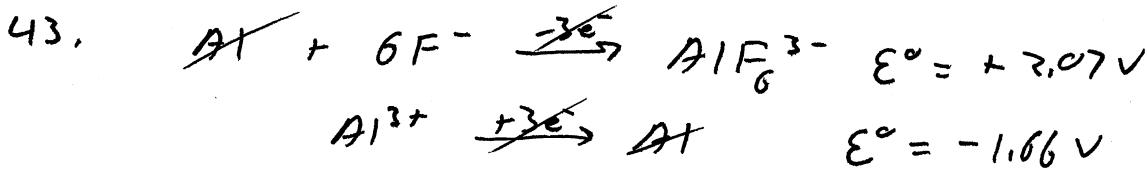


$$E_{cell}^\circ = \frac{-0.77\text{ V}}{\text{Fe}^{2+}\text{ox}} + \frac{1.23\text{ V}}{\text{O}_2\text{red}} = +0.46\text{ V}$$

as shown in
non-graded
part...

$$\Delta G^\circ = -178 \text{ kJ/mol}$$

$$K = 1.32 \times 10^{31}$$



$$\Delta G^\circ = -nFE^\circ$$

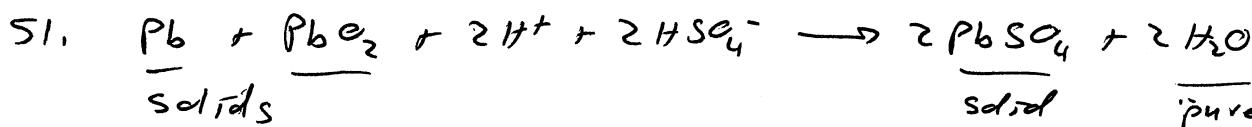
$$= -(3)(96,485 \text{ J/Vmol})(0.41\text{ V})$$

$$= -119 \text{ kJ/mol}$$

$$K = e^{-\Delta G^\circ/RT}$$

$$= e^{-(-119,000 \text{ J/mol})/(8,314 \text{ J/K})(298\text{ K})}$$

$$= 6.35 \times 10^{20}$$



$$\epsilon = 2.04 \text{ V} - \frac{0.0591 \text{ V}}{2} \log \left(\frac{1}{[\text{H}^+]^2 [\text{HSO}_4^-]} \right) \quad \begin{array}{l} \text{"pure" liquid} \\ \text{not included} \\ \text{here} \end{array}$$

a. $[\text{H}^+] = [\text{HSO}_4^-] = 4.5 \text{ M}$

$$\epsilon = 2.04 \text{ V} + 0.077 \text{ V} = 2.12 \text{ V}$$

(For 6 cells in series, 12.7 V)

b. $\Delta G^\circ = -315.9 \text{ kJ/mol} - (253 \text{ K})(263.5 \text{ J/K})$

↑ Note the units! ↑
+ convert before adding!

$$= -382.6 \text{ kJ/mol}$$

$$\epsilon^\circ = - \frac{\Delta G^\circ}{nF}$$

$$= 1.98 \text{ V}$$

c. now we need to use the "proper" version
of the Nernst eqn with all the parameters

$$\epsilon = \epsilon^\circ - \frac{RT}{nF} \ln Q$$

T = 253 K :

$$\epsilon = 1.98 \text{ V} - \frac{(8.314 \text{ J/mol K})(253 \text{ K})}{(2)(96,485 \text{ J/V mol})} \ln \left(\frac{1}{(4.5)^2 (4.5)^2} \right)$$

$$= 2.05 \text{ V}$$

(For 6 of these in series, 12.3 V)

d. That's almost half a volt less overall.

(Of course oil viscosity is a problem also.)

2. Ch 10, 25. a. 1 mol gas, 1.0 L, 5.0 atm

expands isothermally to 2.0 L against no external pressure, so

$$w = 0 \quad \therefore q = 0$$

$$\begin{aligned} q_{\text{rev}} &= \underline{nRT \ln \left(\frac{V_2}{V_1} \right)} \quad \text{we could calculate } T \\ &= PV \ln \frac{V_2}{V_1} \quad (T = \frac{PV}{nR}) \text{ but} \\ &= 5 \text{ atm} \ln \left(\frac{2}{1} \right) \quad PV = nRT \text{ & we} \\ &= 3.47 \text{ L atm} \times \frac{101.3 \text{ J}}{1 \text{ L atm.}} \quad \text{already have } PV! \\ &= 351 \text{ J} \end{aligned}$$

$$T = \frac{(5 \text{ atm})(1 \text{ L})}{(1 \text{ mol})(0.082 \frac{\text{L atm}}{\text{mol K}})} = 61 \text{ K}$$

$$\Delta S = \frac{q_{\text{rev}}}{T} = 5.76 \frac{\text{J}}{\text{K}}$$

$$\Delta S = \underset{P}{nR \ln \frac{V_2}{V_1}} = 5.76 \frac{\text{J}}{\text{K}}$$

$$8.314 \frac{\text{J}}{\text{mol K}}$$

b. $P_i = 2 \text{ atm} \Rightarrow T = 24 \text{ K}$ (rrrrrrr...)

ΔS is the same! $5.76 \frac{\text{J}}{\text{K}}$

$$q_{\text{rev}} = 140 \text{ J}$$

c. $P_i = 15 \text{ atm} \Rightarrow T = 183 \text{ K}$

ΔS is the same! $5.76 \frac{\text{J}}{\text{K}}$

$$q_{\text{rev}} = 1053 \text{ J}$$

same inc. in

"disorder"

results from
less heat

input at low T
& more at

high T

3. 50. See non-graded parts -

$$\begin{aligned} \alpha_f^\circ &= -802.5 \frac{\text{kJ/mol}}{} \quad \rightarrow \quad \Delta G^\circ = -801 \frac{\text{kJ/mol}}{} \\ \Delta S^\circ &= -4 \frac{\text{J/K}}{} \quad \text{---} \quad T = 298 \text{ K} \end{aligned}$$

50. (cont'd)

d. $\Delta H^\circ = -176 \text{ kJ/mol}$ $\Rightarrow \Delta G^\circ = -91 \text{ kJ/mol}$
 $\Delta S^\circ = -284 \frac{\text{J}}{\text{K}}$ $T = 298 \text{ K}$

4, 52. $\Delta H^\circ + \Delta S^\circ$ are normally assumed to be \sim temp-independent
 ΔG° , of course, depends on T —

$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ$$

— how strong/ly T-dep it is depends on the magnitude of ΔS° .

53. $T = 298 \text{ K}$: $\Delta G^\circ = -58.03 \frac{\text{kJ}}{\text{mol}} - (298 \text{ K})(-176.6 \frac{\text{J}}{\text{K}})$
 watch the units!

$$\Delta G^\circ = -5.40 \text{ kJ/mol}$$

$$\Delta G^\circ = 0 \text{ when } \Delta H^\circ = T\Delta S^\circ$$

$$\therefore T = 328.6 \text{ K} = 55.4^\circ\text{C} —$$

above this temp, $-T\Delta S^\circ$ term dominates, so ΔG° is pos; below this temp ΔH° dominates, & ΔG° is neg.

$$90^\circ\text{C} \Rightarrow 363 \text{ K} \quad \Delta G^\circ = +6.08 \text{ kJ/mol}$$

$$-50^\circ\text{C} \Rightarrow 223 \text{ K} \quad \Delta G^\circ = -18.65 \text{ kJ/mol}$$



a. $\Delta G^\circ = -RT \ln K$
 $= -(8.314 \frac{\text{J}}{\text{mol K}})(298 \text{ K}) \ln(1.00 \times 10^{-14})$
 $= +79.9 \text{ kJ/mol}$

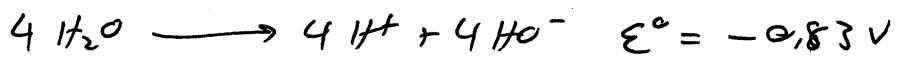
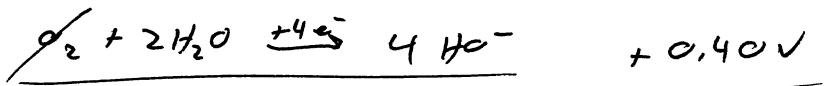
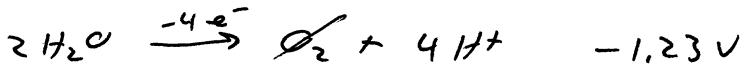
b. $T = 40^\circ\text{C}$

$$K = 2.92 \times 10^{-14}$$

↓

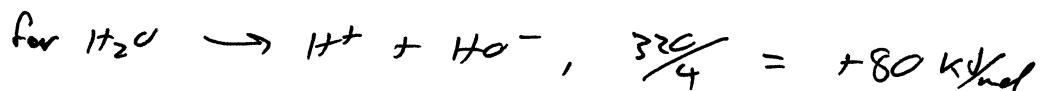
$$\Delta G_{40}^\circ = 81.1 \text{ kJ/mol}$$

5. (cont'd) - didn't we do this in class?



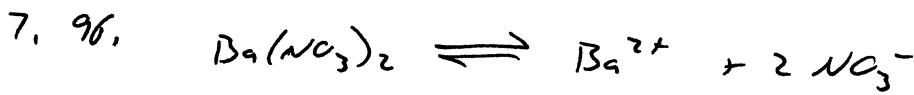
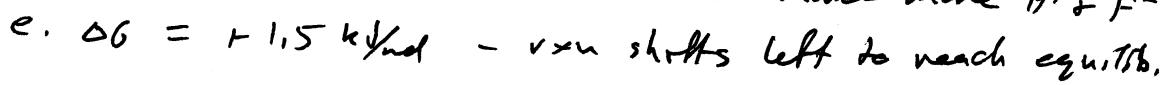
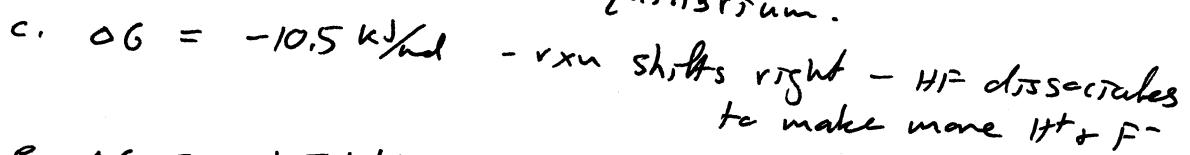
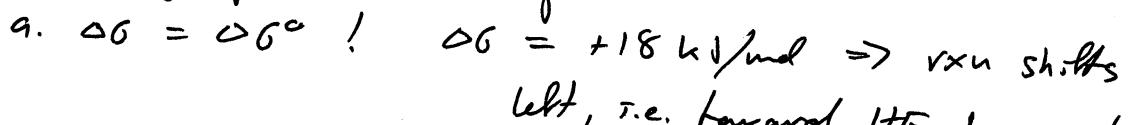
$$\Delta G^\circ = -(4)(96,485 \frac{\text{J}}{\text{mol}\text{V}})(-0.83\text{ V})$$

$$= +320 \frac{\text{J}}{\text{mol}} \quad \text{for the rxn as written!}$$



same as
above!

6. 91. see non-gr. part for set-up.



$$\Delta G^\circ = +18 \frac{\text{kJ}}{\text{mol}} \Rightarrow K_{sp} = e^{-\frac{(18,000 \text{ J/mol})}{(8.314 \frac{\text{J}}{\text{mol}\text{K}})(298\text{K})}} = 7.0 \times 10^{-4}$$



$$T_b = 35^\circ\text{C} = 308\text{K}$$

$$\Delta H_{\text{vap}}^\circ = 27.5 \frac{\text{kJ}}{\text{mol}}$$

$$\Delta S_{\text{vap}}^\circ = \frac{\Delta H_{\text{vap}}^\circ}{T} = \frac{27500 \frac{\text{J}}{\text{mol}}}{308\text{K}} = 89.3 \frac{\text{J}}{\text{mol}\text{K}}$$